

Phase Shifting Interferometry algorithms performance characterization under random stepping errors.

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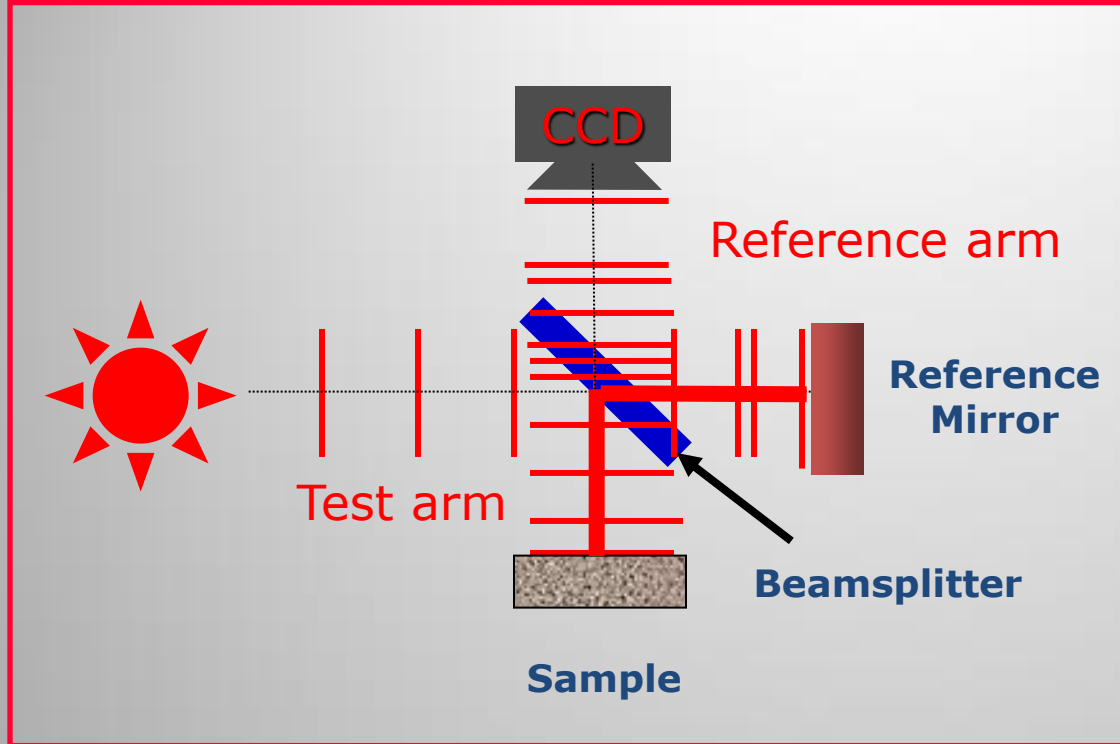
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Brief outlook

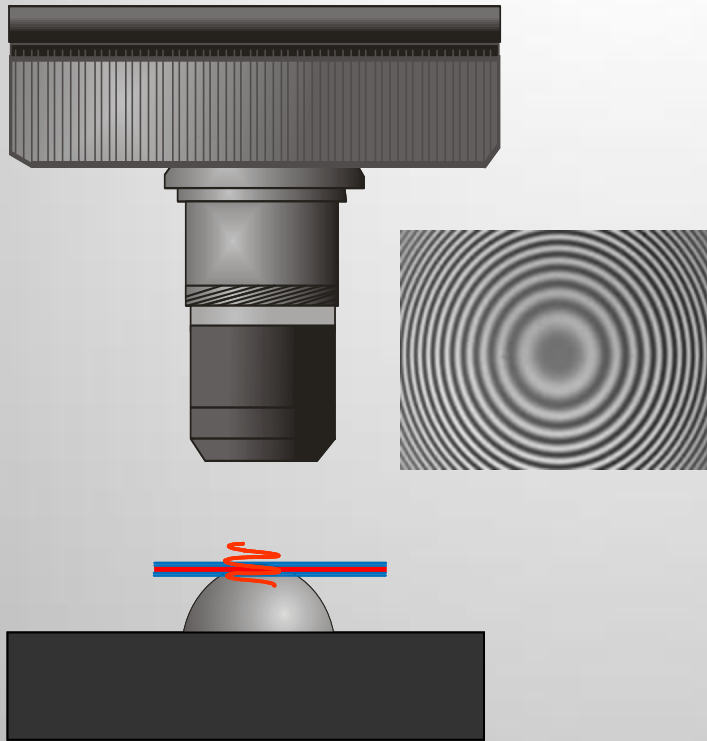
- Laser interferometry is a powerful technique:
 - based on phase estimation from successive measurements.
 - used:
 - at NIF by VISAR (Velocity Interferometer System for Any Reflector).
 - in industry for surface profiling
 - for stellar measurements (JPL).
- The accuracy depends on the precise positioning for data collection.
- Many parallel algorithms were developed to compensate for systematic positioning errors (bias), but no global characterization exists.
- A new quality measure for algorithms with equivalent bias performance and additional random stepping errors is suggested.

Optical interferometer – general principle



- The light from the source is split in two parts and sent on the object and on the reference mirror.
- The reflected beams are recombined.
- The recorded intensity depends upon the difference of the distances traveled by each beam -> constructive or destructive interference.

Phase shifting interferometry (PSI)



- Short scans, monochromatic light (λ).
- Frames are separated by an optical path difference (OPD) less than $\lambda/2$.

Distance measurement

- The recorded intensity by every CCD pixel is the combination of the reference “r” and object “o” beams.

$$I = I_o + I_r + 2\sqrt{I_o I_r} \sin \left[\frac{2\pi}{\lambda} (z_r - z_o) \right]$$

- The reference (or object) position is varied in equal steps (Δ).

$$z_r^{(n)} = z_r^{(0)} + n\Delta$$

- The intensity at every position “n” is given by:

$$\begin{aligned} I_n &= I_o + I_r + 2\sqrt{I_o I_r} \sin \left[\frac{2\pi}{\lambda} (n\Delta) + \frac{2\pi}{\lambda} (z_r^{(0)} - z_o) \right] \\ &\equiv A + B \sin(\omega_0 n + \phi) \end{aligned}$$

- Distance measurement is a problem of **phase detection**.

Algorithms for phase detection

- A very large number designed to account for **systematic** stepping errors .
- Aim to determine a set of $\{a_n, b_n\}$ coefficients such that:

$$\tan(\phi) = \frac{\sum_n a_n I_n}{\sum_n b_n I_n} = \frac{\sum_n a_n [A + B \sin(\omega_0 n + \phi)]}{\sum_n b_n [A + B \sin(\omega_0 n + \phi)]}$$

- Necessary conditions:

$$\sum_n a_n = \sum_n b_n = 0$$

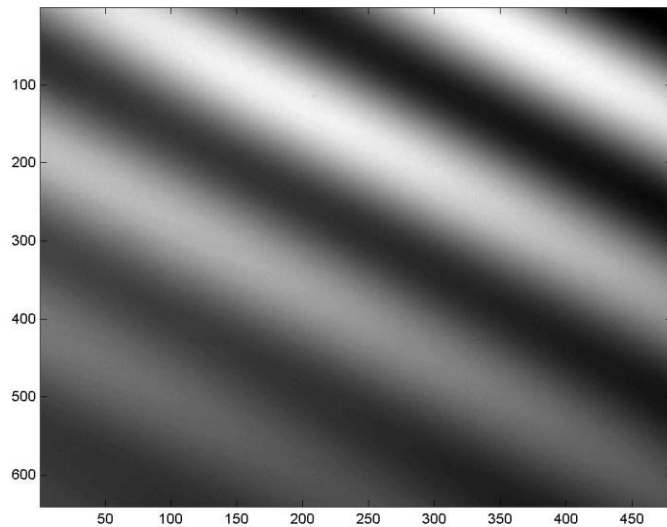
$$\frac{\sum_n a_n \sin(\omega_0 n + \phi)}{\sum_n b_n \sin(\omega_0 n + \phi)} = \frac{\sin(\phi + \zeta)}{\cos(\phi + \zeta)}$$

- Additional conditions can be imposed to compensate **systematic uncertainties** in ω .

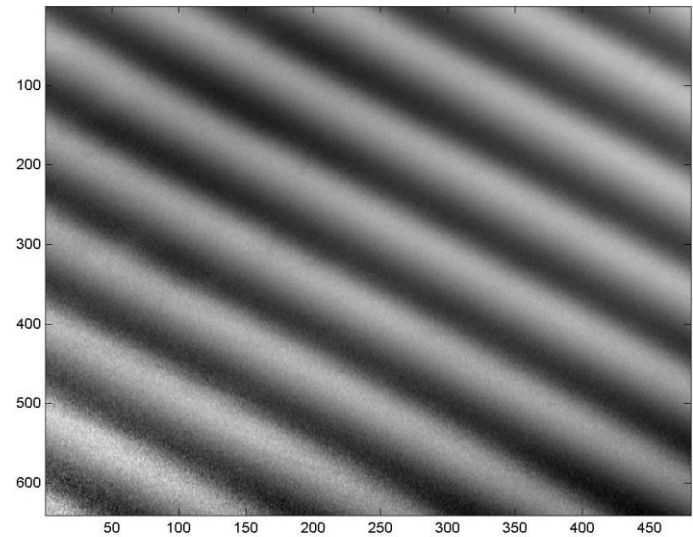
Effects of stepping errors.

- Variations in steps ($\omega_0 \rightarrow \omega_0 + \delta$) lead to errors in the measured phase (**Bias**).

$$\tan(\Delta\phi) = -\frac{r \sin(2\phi)}{1 + r \cos(2\phi)}$$



- One frame from a flat mirror.



- Recovered profile of a flat mirror.

Compensation of step errors – general.

- Specific errors are being addressed by using Fourier approach. Start by correlating the recorded signal $I(z)$ with two unknown functions (f_1, f_2):

$$I(z) = \sum_{n=0}^{\infty} V_n \cos(n\omega_0 z + \phi_n) \longrightarrow \begin{cases} p(z) = I(z) \oplus f_1(z) = \int_{-\infty}^{\infty} I(\zeta) f_1(z + \zeta) d\zeta \\ q(z) = I(z) \oplus f_2(z) = \int_{-\infty}^{\infty} I(\zeta) f_2(z + \zeta) d\zeta \end{cases}$$

$$r = \frac{p(0)}{q(0)} = \frac{\sum_{n=0}^{\infty} V_n [e^{i\phi_n} F_1^*(n\omega_0) + e^{-i\phi_n} F_1^*(-n\omega_0)]}{\sum_{n=0}^{\infty} V_n [e^{i\phi_n} F_2^*(n\omega_0) + e^{-i\phi_n} F_2^*(-n\omega_0)]}$$

- The phase corresponding to the frequency “m” can be retrieved from:

$$\tan(\phi_m) = r$$

if the following conditions are fulfilled:

$$\begin{aligned} F_1^*(n\omega_0) &= F_2^*(n\omega_0) = 0, & n \neq m \\ F_1^*(m\omega_0) &= -iF_2^*(m\omega_0) \end{aligned}$$

Compensation of stepping errors – example.

- Choose:

$$f_1(z) = \sum_{k=0}^N a_k \delta(z - z_k) \quad F_1^*(n\omega_0) = \sum_{k=0}^N a_k^* e^{i(n\omega_0)z_k}$$

$$f_2(z) = \sum_{k=0}^N b_k \delta(z - z_k) \quad F_2^*(n\omega_0) = \sum_{k=0}^N b_k^* e^{i(n\omega_0)z_k}$$

- Then the phase can be recovered from:

$$r = \frac{\sum_{k=0}^N a_k I(z_k)}{\sum_{k=0}^N b_k I(z_k)}$$

- A linear error in stepping corresponds to:

$$\omega_0 \rightarrow \omega_0 + \delta$$

- In the case when the error is small:

$$F_1^*(n\omega_0) = \sum_{k=0}^N a_k^* e^{i(n\omega_0)z_k} [1 + (in z_k) \delta]$$

$$F_2^*(n\omega_0) = \sum_{k=0}^N b_k^* e^{i(n\omega_0)z_k} [1 + (in z_k) \delta]$$

- a set of additional equations for $\{a_n, b_n\}$ necessary to cancel (δ) can be derived.

Algorithm performance characterization.

- A very large number of algorithms have been derived.
- Their performance is currently estimated by the size of the phase error (**bias**) calculated from synthetic data with **specific** sampling errors.
- As of now, no way of characterizing algorithms with equivalent bias performance exists.

$$MSE(\hat{\phi}) \equiv E [(\hat{\phi} - \phi)^2] = [Bias(\hat{\phi}, \phi)]^2 + Var(\hat{\phi})$$

- We suggest as a measure for the global performance the magnitude of the phase variance $Var[\Phi]$ in the presence of completely random stepping errors.
- Critical assumption: **Correct steps -> Correct phase determination!**
(zero bias)

Stochastic analysis.

- Each data point in the signal is given by:

$$I_k = A + B \sin(k\Delta + \alpha_k + \phi) + \epsilon_k$$

$$E[\alpha_k] = \mu_\alpha \quad E[\epsilon_k] = 0$$

$$\text{Cov}[\alpha_k, \alpha_j] = \sigma_\alpha^2 \delta_{k,j} \quad \text{Cov}[\epsilon_k, \epsilon_j] = \sigma_\epsilon^2 \delta_{k,j} \quad \text{Cov}(\alpha_k, \epsilon_j) = 0$$

- Phase estimator:

$$\hat{\phi} = \arctan \left[\frac{\sum_{i=1}^N a_i I_i}{\sum_{j=1}^N b_j I_j} \right] - \zeta$$

- First order error propagation:

$$\mu_{\hat{\phi}} = E[\hat{\phi}] = E \left[\frac{\sum_{i=1}^N a_i I_i}{\sum_{j=1}^N b_j I_j} \right] \approx \left. \frac{\sum_{i=1}^N a_i E[I_i]}{\sum_{j=1}^N b_j E[I_j]} \right|_{\hat{\phi}=\phi}$$
$$\sigma_{\hat{\phi}}^2 = V[\hat{\phi}] \approx \sigma_\alpha^2 \sum_{k=1}^N \left[\frac{\partial \hat{\phi}}{\partial \alpha_k} \right]_{\hat{\phi}=\phi}^2 + \sigma_\epsilon^2 \sum_{k=1}^N \left[\frac{\partial \hat{\phi}}{\partial \epsilon_k} \right]_{\hat{\phi}=\phi}^2$$

Proposed estimator.

- Expected phase variance due to random step errors:

$$E_{\phi}^{step} [Var(\hat{\phi})] = \sigma_{\alpha}^2 \left[\frac{1}{4(S_a^2 + S_b^2)} \sum_{k=1}^N \left\{ \begin{array}{l} (a_k^2 + b_k^2) \\ + \sin(2\zeta) \left[-a_k b_k \cos(2k\Delta) + \frac{a_k^2 - b_k^2}{2} \sin(2k\Delta) \right] \\ + \cos(2\zeta) \left[a_k b_k \sin(2k\Delta) + \frac{a_k^2 - b_k^2}{2} \cos(2k\Delta) \right] \end{array} \right\} \right]$$

- Proposed measure for algorithm performance:

$$T(a_k, b_k, \Delta) \equiv \frac{1}{4(S_a^2 + S_b^2)} \sum_{k=1}^N \left\{ \begin{array}{l} (a_k^2 + b_k^2) \\ + \sin(2\zeta) \left[-a_k b_k \cos(2k\Delta) + \frac{a_k^2 - b_k^2}{2} \sin(2k\Delta) \right] \\ + \cos(2\zeta) \left[a_k b_k \sin(2k\Delta) + \frac{a_k^2 - b_k^2}{2} \cos(2k\Delta) \right] \end{array} \right\}$$

$$S_a \equiv \sum_{k=1}^N a_k \sin(k\Delta) \quad S_b \equiv \sum_{k=1}^N b_k \sin(k\Delta)$$

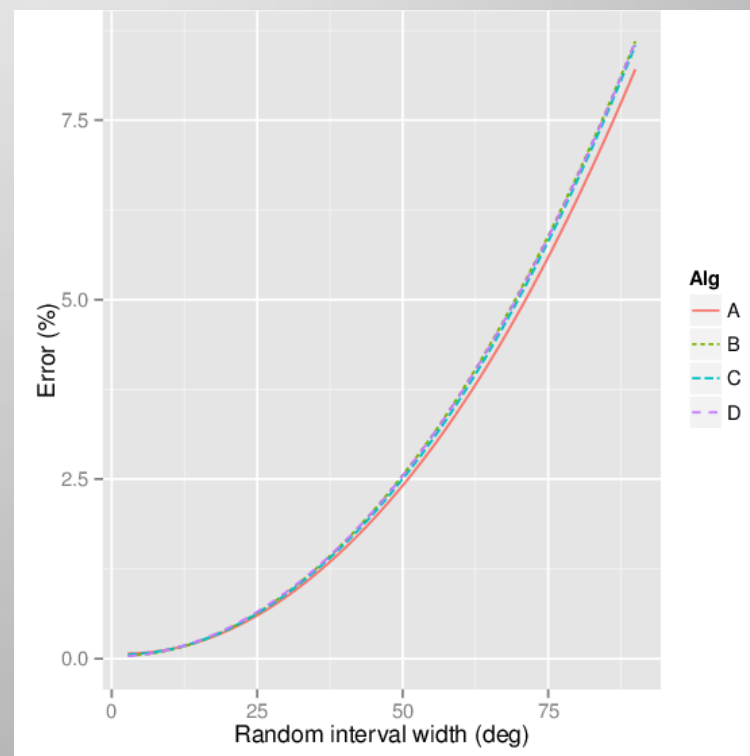
$$C_a \equiv \sum_{k=1}^N a_k \cos(k\Delta) \quad C_b \equiv \sum_{k=1}^N b_k \cos(k\Delta)$$

Synthetic data results.

- Four algorithms were compared

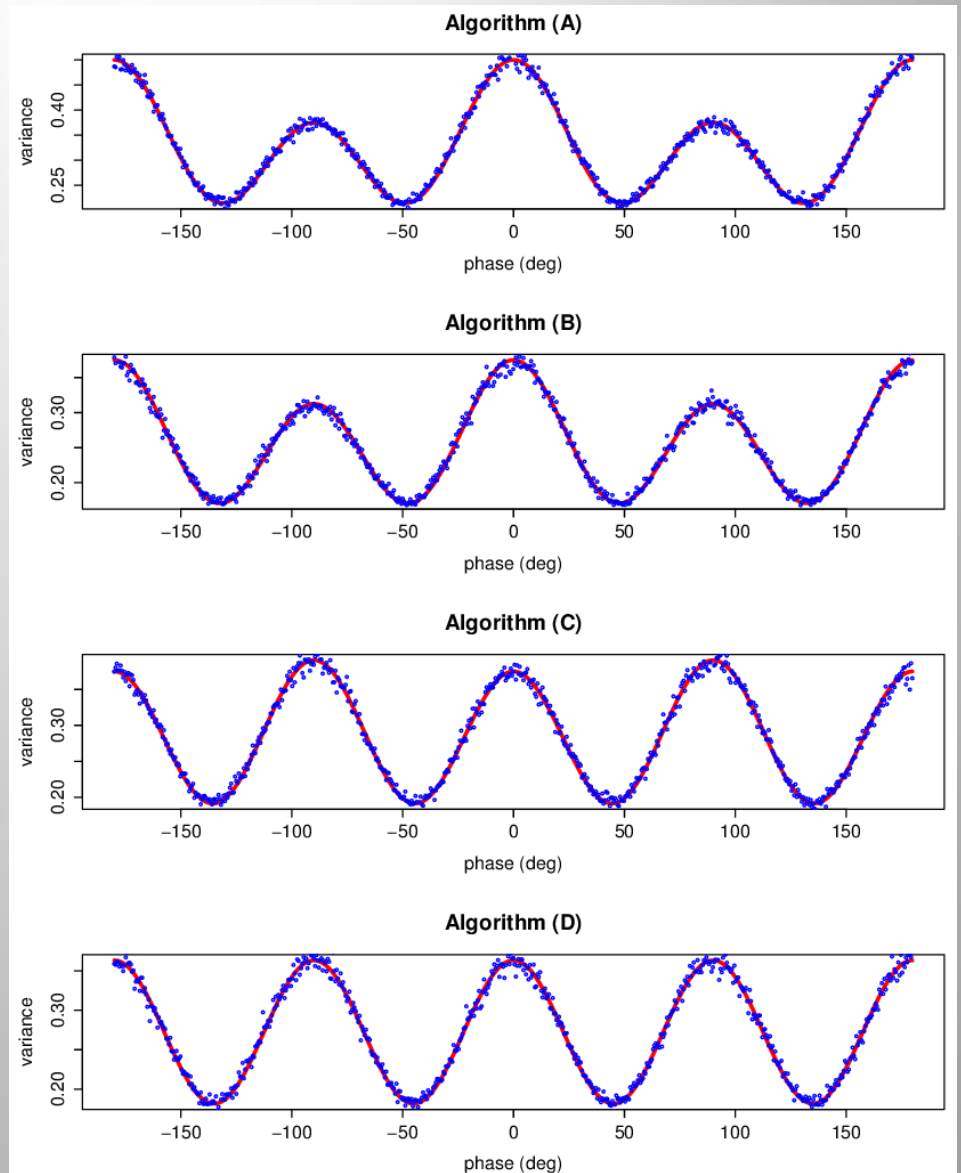
Name	No. frames	Algorithm coefficients	
		a	b
A	5	{0, -2, 0, 2, 0}	{1, 0, -2, 0, 1}
B	7	{0.5, 0, -1.5, 0, 1.5, 0, -0.5}	{0, 1, 0, -2, 0, 1, 0}
C	7	{1, 0, -7, 0, 7, 0, -1}	{0, 4, 0, -8, 0, 4, 0}
D	8	{1, -5, -11, 15, 15, -11, -5, 1}	{1, 5, -11, -15, 15, 11, -5, -1}

- Error (%) between the proposed formula and MC simulation with the size of the step error interval (in degrees).



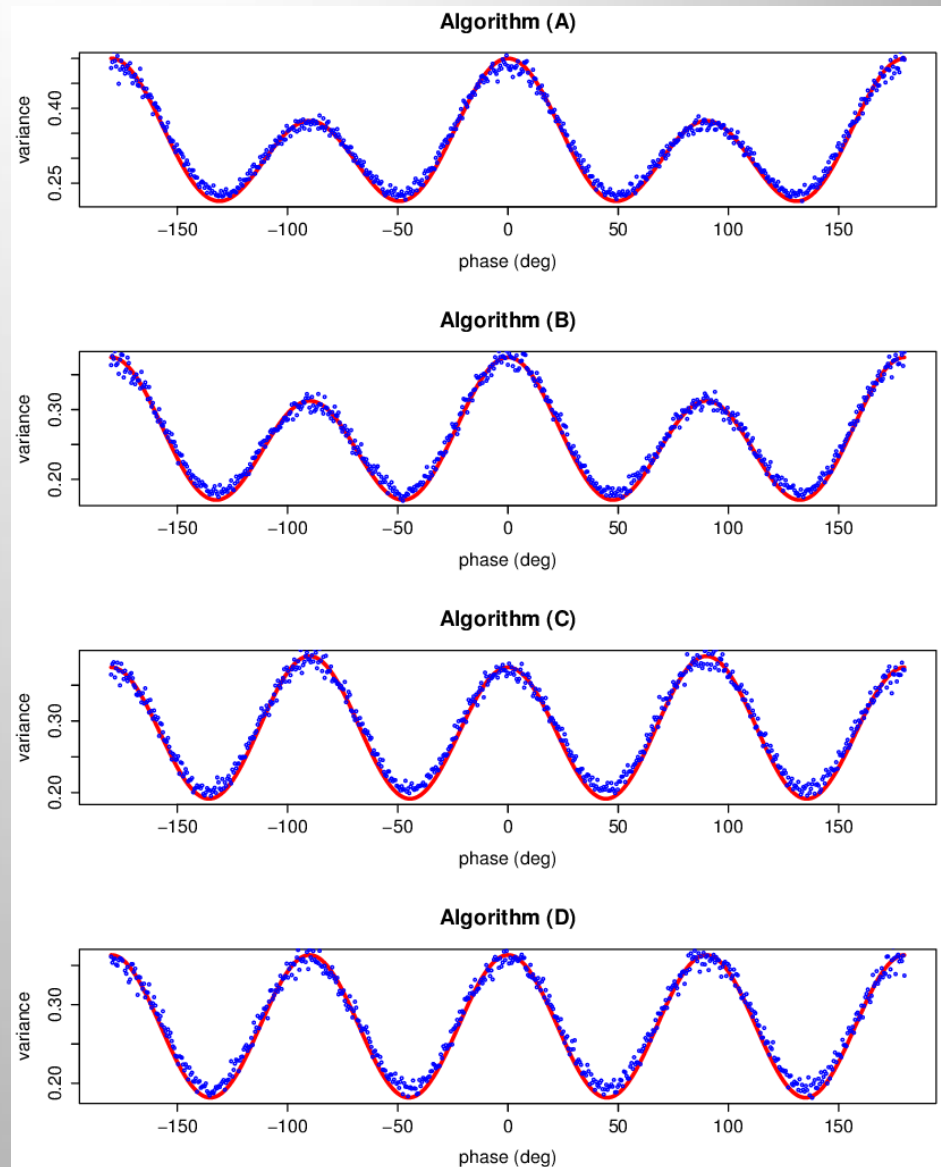
Synthetic data results.

- Predicted (red line) and MC variances (blue dots) as function of signal phase.
- Step error interval = $\pi/10$



Synthetic data results.

- Predicted (red line) and MC variances (blue dots) as function of signal phase.
- Step error interval = $\pi/4$



Algorithm performance comparison.

- No systematic error present.

Alg	No. frames (N)	$T(a_k, b_k, \Delta)$	$U(a_k, b_k, \Delta)$	$N \times T$	$N \times U$
A	5	0.328	0.437	1.64	2.187
B	7	0.258	0.344	1.80	2.41
C	7	0.287	0.383	2.01	2.68
D	8	0.272	0.363	2.18	2.91

- Linear mis-calibration step of 40 deg.

Alg	No. frames (N)	$T(a_k, b_k, \Delta)$	$U(a_k, b_k, \Delta)$	$N \times T$	$N \times U$
A	5	0.467	0.831	2.33	4.16
B	7	0.879	1.572	6.15	11.00
C	7	0.589	1.045	4.12	7.31
D	8	0.645	1.153	5.16	9.22

Conclusion.

- Selection of phase detection algorithm must be done based on:
 - Presence of known systematic errors.
 - Bias compensation performance.
 - Stochastic performance.

